

HANSER



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Injection Mold Design Engineering

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ERRATA

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These are errata for the First Edition of the book published in 2007. The author welcomes errata and other feedback on this book for implementation in future editions.

p. 53-55, Mold Base Cost Estimation: Mass and coefficients were derived for units of lb. Formula and coefficients are self-consistent so result in correct estimation of mold base cost.

p. 61, Table 3.11: Mold maintenance coefficient for hardened surface or tool steel, such as H13, should be 1.2 when used with an unfilled low viscosity plastic.

p. 63, Table 3.13: Columns for hot and cold runners are switched. The corrected table is:

Type of feed system and mold operation	Cycle efficiency factor, <i>f_{cycle efficiency, hot runner}</i>	Cycle efficiency factor, <i>f_{cycle efficiency, cold runner}</i>
Semi-automatic molding with operator removal of molded parts	2.5	3.0
Semi-automatic molding with gravity drop or high speed robotic take-out	1.5	2.0
Fully automatic molding	1.0	1.5

p. 64, Table 3.13: Should be relabeled Table 3.14

p. 99, Equation 5-18: For the power law fitter spreadsheet, the power law viscosity uses the form:

$$\eta = k\dot{\gamma}^{n-1}$$

p. 101, Equation 5-22: The parenthetical term $(1+1/n)$ should be changed to $2+1/n$. The correct formula is:

$$\Delta P = \frac{2kL}{H} \left(\frac{2 \left(2 + \frac{1}{n} \right) \bar{v}}{H} \right)^n = \frac{2kL}{H} \left(\frac{2 \left(2 + \frac{1}{n} \right) \dot{V}}{WH^2} \right)^n$$

p. 202, Equation: 9.4: A factor of $4/\pi$ should be included. The correct formula is:

$$T_{z=0}(t) = T_{coolant} + \frac{4}{\pi} (T_{melt} - T_{coolant}) \sum_{m=0}^{\infty} \frac{(-1)^m}{2m+1} e^{-\frac{\pi^2(2m+1)^2 \alpha}{h^2} t}$$

p. 278, Equation 11-16: The minimum pin radius for buckling is given by:

$$R > \left(\frac{F_{pin} L^2}{15.8E} \right)^{\frac{1}{4}}$$

leading to a pin diameter of 1.33 mm in the subsequent example.